TABLE 1 α -y TRANSFORMATION TEMPERATURES OF IRON AND IRON ALLOYS AT 20, 40 and 60 kb

| Pressure | | 20 kb | | | 40 kb | | | 60 kb | | |
|---|--|---|-------------------|-------------------|-------------------|-------------------|---------------------|-------------------|-------------------|-----------------------|
| Temperature change during transformation | direction up-down average rate °C/min. | | | av -y Trans | formati | on Ter | av mperatur | res, °C | <u></u> | av |
| Alloy Fe-X(weight per cent of minor element) | | | | | | | | | | |
| Fe(pure) | 8-12 | 786 | 761 | 773 | 691 | 657 | 674 | 636 | 581 | 609 |
| Fe-Al (0.54) Fe-Al (0.75) | 8-12 8-12 | 836 865 | 793 807 | 814 836 | 721 733 | 676 683 | 699 708 | 669 67£ | 618 618 | 644 648 |
| Fe-Cr (1.09) Fe-Cr (2.95) Fe-Cr (9.49) | 8-11 8-12 30-50 | 770 766 742 | 750 728 642 | 760 747 692 | 687 676 667 | 640 606 429 | 663 641 548 | 631 640 | 566 391 | 598 490 |
| Fe-Mn (1.07) Fe-Mn (2.85) | 9-16 9-12 | 765 576 | 708 715 | 736 645 | 676 638 | 592 433 | 634 5 3 6 | | | |
| Fe-Co (10.2) Fe-Co (19.9) Fe-Co (39.6) | 30-50 8-12 15-25 | 810 891 945 | 781 876 933 | 796 883 939 | 726 837 902 | 694 816 885 | 710 827 893 | 683 805 870 | 630 778 846 | 6.56(a) 792 858 |
| Fe-Ni (1.07) Fe-Ni (3.06) Fe-Ni (10.0) | 8-12 8-16 22-31 | 766 736 641 | 724 662 460 | 745 698 550 | 681 655 577 | 629 564 327 | 655 610 452 | 627 520 | 545 168 | 585 344(b) |
| | | (a) Extrapolated from 52 kb.(b) Extrapolated from 53 kb. | | | | | | | | |

a pure iron standard showed a very much smaller change in slope. This apparent discrepancy needs further investigation.

Both of these Fe-Al alloys were utilized as secondary standards in later duplex DTCA runs, where the use of iron would have resulted in the standard transition being too close to that of the second material. Particularly, Fe-Al was used with the 1 percent alloys of Mn, Cr and Ni in iron, and with certain Fe-C runs at the higher pressure.

- (b) Iron-Manganese Alloys. The data for two Fe-Mn alloys containing 1.0 and 3.0 percent Mn are shown in Fig.6 and Table 1. The average temperature curves for both alloys appear to be smooth in the region up to 45 kb, except for the scatter from different runs on the 3 percent alloy. However, because of the very large hysteresis in the temperature in these latter data, the average temperature data may not be very accurate; it would seem inadvisable to attribute any significance to apparent changes in slope.
- (c) Iron-Chromium Alloys. The data for three Fe-Cr alloys containing 1, 3 and 10 percent Cr are shown in Fig.7 and Table 1. All of the average temperature curves appear smooth, with no significant changes in slope at any point. The 1 percent curve follows closely parallel to the curve for pure iron. The 3 percent curve departs downward at the higher pressures while the 10 percent curve veers upward at these pressures. This behavior may be related to the expansion of the gamma loop at higher pressures; with more data, par-

ticularly with a 20 percent alloy, a more complete analysis could be made in this direction.

- (d) Iron-Nickel Alloys. The data for three Fe-Ni alloys containing 1, 3 and 10 percent Ni are shown in Fig.8 and in Table 1. All of the average temperature curves appear smooth, with no significant changes in slope at any point. In comparison to the corresponding Fe-Cr alloys, the Fe-Ni alloys transform at lower temperatures and with larger hystereses. Both kinetics and the width of the respective two-phase regions probably make this difference.
- (e) Iron-Cobalt Alloys. The data for three Fe-Co alloys containing 10, 20 and 50 percent cobalt are shown in Fig.9 and Table 1. All of these average temperature Fe-Co curves appear smooth with no significant changes in slope. However, the 20 percent data require some additional comment. At 26 kb and at 28 kb, a second transformation was observed at 796 and 788 C, about 70 deg lower than the α - ν transformation. The originand nature of this additional apparent transformation is unknown, and warrants further investigation.

The α - γ transformations in all of the Fe-Co alloys proceeded with the lowest hystereses of any of the materials studied. The reason for the low hysteresis may be surmised by inspection of the Fe-Co phase diagram. A maximum temperature for the transformation is recorded at 45 percent Co, and at this point the vertical (along the temperature axis) distance separating the two phases, alpha and gamma, should be nil, with a congruent

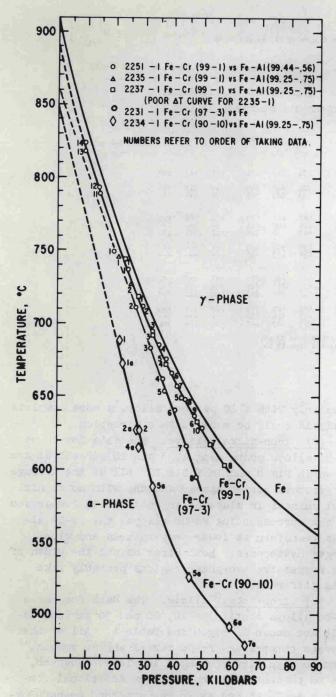


Fig. 7 P-T plots for α - γ transformations in Fe-Cr alloys. Average temperature curves

change in phase. The observation of the lowest hysteresis with the 60-40 alloy agrees with this concept.

The extrapolation of the high-pressure α - γ data usually fits in reasonably well with the atmospheric-pressure data. For the Fe-Co (60-40) alloy, however, where some of the best low-pressure data were obtained, the extrapolation to 972 C was 14 deg lower than that recorded in the literature. A second discrepancy appeared later

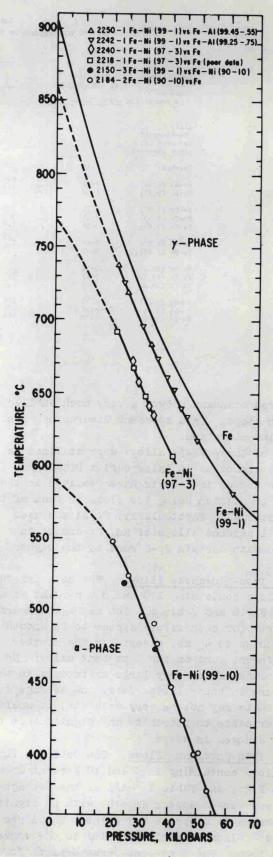


Fig. 8 P-T plots for α - √ transformations in Fe-Ni alloys. Average temperature curves